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WHY5640

Subminiature Temperature Controller

GENERAL DESCRIPTION:

The WHY5640 is a general purpose analog PI (Proportional, Integral) control loop for use in thermoelectric or resistive heater temperature control applications. The WHY5640 maintains precision temperature regulation using an active resistor bridge circuit that operates directly with thermistors or RTD temperature sensors. Supply up to 2.2 Amps of heat and cool current to your thermoelectric from a single +5 Volt power supply.

Connect two or more WHY5640 units together and drive higher output currents.









Component Symbol	Purpose	Page Reference
C	Integrator Time Constant Adjust Capacitor (PI)	12
R _A	Current Limit Set Resistor (Limit A)	6
R _B	Current Limit Set Resistor (Limit B)	6
R _G	Integrator Time Constant Adjust Resistor (PI)	12
R _L	Proportional Gain Adjust Resistor (PI)	12
R _s	Setpoint Resistor	7
R _τ	Thermistor	7

 $\rm V_{s}$ and $\rm V_{\rm \tiny DD}$ may be separate supplies or a single supply.

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ELECTRICAL AND OPERATING SPECIFICATIONS

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ABSOLUTE MAXIMUM RATIN RATING	IGS	SYMBOL	VALUE	UNI	т	
Supply Voltage 1 (Voltage on Pin 8)		V _{DD}	+5 to +26	Volts	S DC	
Supply Voltage 2 (Voltage on Pin 10	V _S	+4.5 to +30	Volts	Volts DC		
Output Current (See SOA Chart)	I _S	±2.2	Amp	Amperes		
Power Dissipation, T _{AMBIENT} = +25°0	C	P _{MAX}	9	Watt	Watts	
Operating Temperature, case		T _{OPR}	-40 to +85	°C		
Storage Temperature		T _{STG}	-65 to +150	°C		
PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNITS	
TEMPERATURE CONTROL						
Short Term Stability, 1 hour	$T_{SET} = 25^{\circ}C$ using 10 k Ω thermistor	r 0.001	0.005	0.01	°C	
Long Term Stability, 24 hour	$T_{SET} = 25^{\circ}C$ using 10 k Ω thermistor	r 0.003	0.008	0.01	°C	
Setpoint vs. Actual Temp Accuracy	$T_{SET} = 25^{\circ}C$ using 10 k Ω thermistor	r	<1%			
Control Loop		P	PI			
P (Proportional Gain)		1		100	A/V	
I (Integrator Time Constant)		1		10	Sec.	
OUTPUT						
Current, peak, see SOA chart			± 2.0	± 2.2	Amps	
Compliance Voltage, Pin 9 to Pin 13	Full Temp. Range, I _S = 100 mA	V _S - 0.7	VS - 0.5		Volts	
Compliance Voltage, Pin 9 to Pin 13	Full Temp. Range, I _S = 1 Amp	V _S - 1.2	V _S - 1.0		Volts	
Compliance Voltage, Pin 9 to Pin 13	Full Temp. Range, I _S = 2 Amps	VS - 1.6	V _S - 1.4		Volts	
POWER SUPPLY						
Voltage, V _S		4.5		30	Volts	
Voltage, V _{DD}		5		26	Volts	
Current, V _S supply, Quiescent			45	90	mA	
Current, V _{DD} supply, Quiescent			10	15	mA	
INPUT						
Offset Voltage, initial	Pin 5 and 7		1	2	mV	
Bias Current	Pins 5 and 7, T _{AMBIENT} = 25°C		20	50	nA	
Offset Current	Pins 5 and 7, $T_{AMBIENT} = 25^{\circ}C$		2	10	nA	
Common Mode Range	Pins 5 and 7, Full Temp. Range	0		1.5- _{חח} V	V	
Common Mode Rejection	Full Temperature Range	60	85	00	dB	
Power Supply Rejection	Full Temperature Range	60	80		dB	
Input Impedence			500		kΩ	
THERMAL						
Heatspreader Temperature Rise	T _{AMBIENT} =25°C	28	30	33	°C/W	
Heatspreader Temperature Rise	With WHS302 Heatsink, WTW002	18	21.5	25	°C/W	
	Thermal Washer					
Heatspreader Temperature Rise	With WHS302 Heatsink, WTW002	3.1	3.4	3.9	°C/W	
	Thermal Washer, and 3.5 CFM Far	1				

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PIN DESCRIPTIONS				
DIN #	DIN		FUNCTION	
1	AGND	Analog Ground	The analog ground connection is internally connected to Pins	
			11 and 12 (the power supply ground connections) and	
			eliminates grounds loops for stable operation of the sensor	
			amplifier bridge and limit current resistors.	
2	LIMB	LIMIT B	A resistor connected between Pin 2 (LIMB) and Pin 1 (AGND)	
			sets the maximum output current drawn from the Pin 10 (V.) supply	
			input and delivered to Pin 13 (OUTB). This is cooling current when	
			used with NTC sensors.	
3	LIMA	LIMIT A	A resistor connected between Pin 3 (LIMA) and Pin 1 (AGND)	
			sets the maximum output current drawn from the Pin 10 (V.) supply	
			input and delivered to Pin 9 (OUTA). This is heating current when	
			used with NTC sensors. Also connect integrator capacitor C to	
			Pin 3 (LIMA) when operating the WHY5640 as a standard PI	
			controller.	
4	BUFA	BUFFER A	Connect Pin 4 (BUFA) to Pin 3 (LIMA) of another WHY5640	
			when operating the devices in a master/slave configuration.	
5	PI	Proportional Gain/ Integrator	When using the WHY5640 as a standard PI controller, connect	
		Common	one end of the proportional gain resistors R_g and R_L to Pin 5 (PI).	
6	ERR	Temperature Error Input	When using the WHY5640 as a standard PI controller, connect	
			one end of the proportional gain resistor R _g to Pin 6 (ERR).	
7	SENS	Sensor and Setpoint Input	Pin 7 (SENS) is the common sensor bridge amplifier connection	
			for the sensor, R_{τ} , and setpoint, R_s , resistors.	
8	VDD	Control Electronics Supply	Power supply input for the WHY5640's internal control	
		Input	electronics. Supply range input for this pin is +5 to +26 Volts DC.	
9	OUTA	Thermoelectric Output A	Connect Pin 9 (OUTA) to the negative terminal on your	
			thermoelectric when controlling temperature with Negative	
			Temperature Coefficient thermistors. Connect Pin 9 (OUTA) to	
			the positive thermoelectric terminal when using Positive	
			Temperature Coefficient RTDs.	
10	VS	Power Drive Supply Input	Provides power to the WHY5640 H-Bridge Power Stage.	
			Supply range input for this pin is +4.5 to +30 Volts DC. The	
			maximum current drain on this terminal should not exceed	
			2.5 Amps.	
11	PGND	Power Drive Supply Ground	Connect the V_S power supply ground connection to Pin 11	
			(PGND). Pin 11 (PGND) and Pin 12 (CGND) are internally	
			connected.	
12	CGND	Control Electronics Supply	Connect the V _{DD} supply ground connection to Pin 12 (CGND).	
		Ground	Pin 12 (CGND) and Pin 11 (PGND) are internally connected.	
13	OUTB	Thermoelectric Output B	Connect Pin 13 (OUTB) to the positive terminal on your	
			thermoelectric when controlling temperature with Negative	
			Temperature Coefficient thermistors. Connect Pin 13 (OUTB)	
			to the negative thermoelectric terminal when using Positive	
			Temperature Coefficient RTDs.	
14	BUFB	Buffer B	Connect Pin 14 (BUFB) to Pin 2 (LIMB) of another WHY5640	
			when operating the devices in a master/slave configuration.	
			NHV5640 to the WTC3243. The position of Pin 4 on the	
WHY5640 is reversed (or mirrored) relative to the position of Pin 1 on the WTC3243.				

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SAFE OPERATING AREA & HEATSINK REQUIREMENTS **Caution:**

Do not exceed the Safe Operating Area (SOA). Exceeding the SOA voids the warranty.

To determine if the operating parameters fall within the SOA of the device, the maximum voltage drop across the controller and the maximum current must be plotted on the SOA curves.

These values are used for the example SOA determination:

 $V_s = 12$ volts

 $V_{LOAD} = 5$ volts $I_{LOAD} = 1$ amp These values are determined from the specifications of the TEC or resistive heater

Follow these steps:

- 1. Determine the maximum voltage drop across the controller, $V_s V_{LOAD}$, and mark on the X axis. (12 volts - 5 volts = 7 volts, Point A)
- Determine the maximum current, I_{LOAD}, through the controller and mark on the Y axis: (1 amp, Point B)
- 3. Draw a horizontal line through Point B across the chart. (Line BB)
- 4. Draw a vertical line from Point A to the maximum current line indicated by Line BB.
- 5. Mark Vs on the X axis. (Point C)
- 6. Draw the Load Line from where the vertical line from point A intersects Line BB down to Point C.

Refer to the chart shown below and note that the Load Line is in the Unsafe Operating Areas for use with no heatsink (1) or the heatsink alone (2), but is outside of the Unsafe Operating Area for use with heatsink and Fan (3).

An online tool for calculating your load line is at <u>http://www.teamWavelength.com/support/calculator/soa/soatc.php</u>.



OPERATION

1. CONFIGURING HEATING AND COOLING CURRENT LIMITS

Refer to Table 1 to select appropriate resistor values for $R_{_{\!A}}$ and $R_{_{\!B}}$

Setting Current Limits Independently Using Trimpots

The 5 k Ω trimpots shown in Figure 3 adjust the maximum output currents from 0 to 2.3 Amps

Heat and Cool Current Limits

APPROXIMATE VALUE OF CURRENT LIMIT RESISTOR Rc vs MAXIMUM OUTPUT CURRENT



Table 1

Current Limit Set Resistor vs Maximum Output Current

Maximum Output Current (Amps)	Maximum Output Current (kΩ) R _A , R _B		
0.0	1.60		
0.1	1.69		
0.2	1.78		
0.3	1.87		
0.4	1.97		
0.5	2.08		
0.6	2.19		
0.7	2.31		
0.8	2.44		
0.9	2.58		
1.0	2.72		
1.1	2.88		
1.2	3.05		
1.3	3.23		
1.4	3.43		
1.5	3.65		
1.6	3.88		
1.7	4.13		
1.8	4.42		
1.9	4.72		
2.0	5.07		
2.1	5.45		
2.2	5.88		
2.3	6.36		

Figure 4

Independently Adjustable Heat and Cool Current Limits



Figure 3 Fixed Heat and Cool Current Limits



2. RESISTIVE HEATER TEMPERATURE CONTROL

The WHY5640 can operate resistive heaters by disabling the cooling output current. When using Resistive Heaters with NTC thermistors, connect Pin 3 (LIMA) to Pin 1 (AGND) with a 1.5 k Ω resistor.

Connect Pin 2 (LIMB) to Pin 1 (AGND) with a 1.5 k Ω resistor when using RTDs, LM335 type and AD590 type temperature sensors with a resistive heater.

3. DISABLING THE OUTPUT CURRENT

The output current can be enabled and disabled, as shown in Figure 5, using a DPST (Double Pole–SingleThrow) switch.

4. OPERATING WITH THERMISTOR SENSORS

Figure 6 illustrates how to connect the WHY5640 for operation with NTC (Negative Temperature Coefficient) thermistors.

Connect a setpoint resistor, R_S , (or trimpot) across Pins 1 (AGND) and 7 (SENS). Connect the thermistor, R_T across Pins 6 (ERR) and 7 (SENS).

Select setpoint resistor, R_S, equal to the thermistor resistance at the desired operating temperature.

When the setpoint resistor, R_S , and thermistor, R_T , are equal resistance values the Sensor Bridge Amplifier is balanced and the voltage on Pin 6 (ERR) will equal 1 Volt with reference to Pin 1 (AGND).

If the setpoint resistor, R_S , is larger than the thermistor resistance, R_T , then the control loop will produce a cooling current since the temperature sensed by the thermistor is above (hotter than) the setpoint temperature.

If the setpoint resistor, R_S , is smaller than the thermistor resistance, R_T , then the control loop will produce a heating current since the temperature sensed by the thermistor is below (cooler than) the setpoint temperature.

Figure 5 **Disabling Output Current** $\mathsf{R}_{\scriptscriptstyle\mathsf{B}}$ -1.5 kΩ 1.5 kΩ ENABLE DPST SWITCH DISABLE R, -1.5 kΩ 1.5 kΩ R_{A} 2 WHY5640 AGND LIMA LIMB Figure 6 Thermistor Operation SETPOINT TRIMPOT THERMISTOR R R₊ AGND SENS ERR WHY5640 +0.5 V SENSOR BRIDGE AMPLIFIER

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5. USING AN EXTERNAL SETPOINT VOLTAGE WITH THERMISTOR SENSORS

Figure 7 illustrates how to connect the WHY5640 for operation with NTC (Negative Temperature Coefficient) thermistors using an external setpoint voltage to control the desired operating temperature. This setup is useful when operating the WHY5640 in a DAC controlled system.

Equation 1 illustrates how to determine the setpoint voltage, V_{IN} , given a desired thermistor resistance (temperature).

Resistor, R_1 , is a fixed resistance value that can be used to scale or adjust the setpoint voltage, V_{IN} , allowing control above and below the ambient temperature. In most applications select resistor R_1 equal to two times the desired operating thermistor resistance, R_T .

NOTE: Pin 9 (OUTA) and Pin 13 (OUTB) must be swapped to maintain the proper heating and cooling current polarity through the thermoelectric. Pin 9 (OUTA) becomes the heating current sink and Pin 13 (OUTB) becomes the cooling current sink.

Example 1 demonstrates how to use an external voltage setpoint to control a 10 k Ω thermistor from a range of 20 k Ω to 0 k Ω .

Figure 8 illustrates the setpoint voltage, V_{IN} , versus thermistor resistance, R_T , for Example 1.



Using a $10k\Omega$ Thermistor with External Voltage Control



Figure 7

External Voltage Control Using Thermistor Sensors



NOTE 1: If multiple units are controlled by the buffered op-amp, a 100 Ω resistor from the op-amp output to ground must be added.

Equation 1

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Voltage Controlled Setpoint Using Thermistors

$$V_{\rm IN} = 0.5 - \frac{R_{\rm T}}{2R_{\rm 1}}$$

Figure 8

Example 1 Setpoint Voltage vs Thermistor Resistance



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6. OPERATING WITH RTD SENSORS

Figure 9 illustrates how to connect the WHY5640 for operation with PTC (Positive Temperature Coefficient) RTD sensors (Resistance Temperature Device). Resistors, R₂, should be chosen large enough to prevent self heating of the RTD due to the current flowing through it.

Select setpoint resistor, R_S , equal to the RTD resistance, R_{RTD} , at the desired operating temperature.

When the setpoint resistor, R_S , and RTD, R_{RTD} , are equal in value the Sensor Bridge Amplifier is balanced and the voltage on Pin 6 (ERR) will equal 1 Volt with reference to Pin 1 (AGND).

If the setpoint resistor, R_S , is larger than the RTD resistance, R_{RTD} , then the control loop will produce a heating current since the temperature sensed by the RTD is below (cooler than) the setpoint temperature.

If the setpoint resistor, R_S , is smaller than the RTD resistance, R_{RTD} , then the control loop will produce a cooling current since the temperature sensed by the RTD is above (hotter than) the setpoint temperature.

7. USING AN EXTERNAL SETPOINT VOLTAGE WITH RTD SENSORS

Figure 10 illustrates how to connect the WHY5640 for operation with PTC (Positive Temperature Coefficient) RTD sensors using an external setpoint voltage to control the desired operating temperature. This setup is useful when operating the WHY5640 in a DAC controlled system.

Equation 2 illustrates how to determine the set point voltage, $V_{\rm IN}$, given a desired RTD resistance (temperature).

Resistor, R_2 , is a fixed resistance value that can be used to scale or adjust the setpoint voltage, V_{IN} , allowing control above and below the ambient temperature. In most applications select resistor, R_2 , equal to two times the desired operating RTD resistance, R_{RTD} .





Figure 10 External Voltage Control Using RTD Sensors



Equation 2

Voltage Controlled Setpoint Using RTD Sensors

$$V_{\rm IN} = 0.5 - \frac{R_{\rm RTD}}{2R_2}$$

Example 2 demonstrates how to use an external voltage setpoint to control a 100 Ω RTD from a range of 0 Ω to 200 Ω .

Figure 11 illustrates the setpoint voltage, V_{IN} , versus RTD resistance, R_{RTD} , for Example 2.

Example 2

Using a 100 Ω RTD with External Voltage Control



8. OPERATING WITH AD590 AND LM335 SENSORS

Figure 12 illustrates how to connect the WHY5640 for operation with PTC (Positive Temperature Coefficient) linear sensors AD590 and LM335.

Equation 3 illustrates how to determine the setpoint resistance, R_S , given a desired operating temperature measured in Celsius.

Resistor, R_3 , is a fixed resistance value that can be used to scale or adjust the setpoint resistor, R_s . Select resistor R_3 equal to 10 k Ω for most applications.

Equation 3

AD590 and LM335 Setpoint Resistance Calculation

 $R_{S} = 2R_{3}[0.5 - (273.15 + T_{CELSIUS})(1mV / Kelvin)]$













Example 3 Using an AD590 Example



Example 3 demonstrates how to use an AD590 to control from -50° C to $+150^{\circ}$ C.

Figure 13 illustrates the setpoint resistance, V_{IN} , versus AD590 temperature, for Example 3.

9. MONITORING SETPOINT AND ACTUAL SENSOR VOLTAGES

Figure 13 illustrates how to configure the WHY5640 so the setpoint and actual sensor voltages can be monitored externally.

The WHY5640 internal sensor bridge amplifier becomes balanced (or Pin 6 (ERR) equals 1 Volt) when the sensor voltage equals the setpoint voltage in Figure 14.

The circuit shown in Figure 14 uses a constant current source to produce a sensing current through the resistive temperature sensors resulting in a sensor voltage. A typical sensing current for 20 k Ω and lower thermistors is 100 μ A. For thermistors higher than 20 k Ω use 10 μ A. RTDs require a sensing current of 1 mA.

Note: PTC (Positive Temperature Coefficient) sensors such as RTD sensors, the AD590, and the LM335 require that the output Pins 9 (OUTA -) and 13 (OUTB +) be reversed from the connection diagram on page 2 (Figure 2) to produce the proper cooling and heating currents through the thermoelectric.

When using a 10K Thermistor, per Figure 14, connect the TEC as follows:

 $\begin{array}{rcl} \text{OUTPUT B+} & \longrightarrow & \text{TEC -} \\ \text{OUTPUT A-} & \longrightarrow & \text{TEC +} \end{array}$



Resistance vs AD590 Temperature



Figure 14

Monitor Setpoint and Actual Sensor Voltages



10. ADJUSTING THE CONTROL LOOP PROPORTIONAL GAIN & INTEGRATOR TIME CONSTANT

The control loop parameters are set by the values of two resistors and a capacitor (R_{g} , R_{L} , and C_{L} ; refer to page 2). All three components interact to set the proportional gain and the integrator time constant.

Recommended values for the three components are shown in Table 2 for common sensor and load combinations. A "fast" load can change temperature quickly; conversely a "slow" load is slower to respond to temperature change commands.

Equations for determining the proportional gain and integrator time constant are also provided in order to tune the controller to a variety of load conditions not covered in Table 2.

The relationship between the three components is summarized by the gain-integrator product, k_{τ} , in Equation 6.

Equation 4

Calculating the Proportional Gain, \mathbf{k}_{P}

$$k_{p} = 4 \left(\frac{R_{L}}{R_{G}} \right) amps / volt$$

Equation 5

Calculating the Integrator Time Constant, t_c

$$t_{c} = \left(\frac{R_{G}C_{L}}{4} \right)$$
 seconds

Equation 6

Relationship between k_{P} , t_{C} and k_{T}

$$k_{T} = k_{P}t_{C}$$
 amp•seconds / volt

Table 2

Recommended Gain and Integrator Values

Sensor Type/ Thermal Load Speed	Gain [k _P]	Integrator Time Constant [t _c , seconds]	R _G	RL	CL
Thermistor / Fast	5	3	800 kΩ	1.0 MΩ	15 µF
Thermistor / Slow	20	4.5	400 kΩ	2.0 MΩ	47 µF
RTD / Fast	50	0.53	144 kΩ	1.8 MΩ	15 µF
RTD / Slow	100	1	88 kΩ	2.2 MΩ	47 µF
AD590 or LM335 / Fast	20	1	400 kΩ	2.0 MΩ	10 µF
AD590 or LM335 / Slow	50	4.5	320 kΩ	4.0 MΩ	15 µF

Equation 6 can be related to component values by algebraic substitution, as shown in Equation 7.

Equation 7

Relating k_{τ} to component values

$$k_{T} = C_{L}R_{L}$$
 amp•seconds / volt

The value of R_{g} is then calculated by using either Equation 8 or Equation 9:

Equation 8

Relating k_{τ} to component values

$$R_{G} = \left(\frac{4R_{L}}{k_{P}}\right) \quad ohms$$

Equation 9

Relating k_{τ} to component values

$$R_{_{G}} = \left(\frac{4t_{_{C}}}{C_{_{L}}}\right) ohms$$

When calculating component values, keep in mind these points:

- As k_T becomes larger, choosing component values becomes more difficult because larger C_L values are required.
- 2. Keep R_{L} as small as possible; higher values of R_{L} are more noisy, and values above 4 M Ω will impact temperature control stability.
- 3. As R_{L} becomes smaller, C_{L} must be larger. Use a non-polarized capacitor for C_{L} ; we recommend a ceramic capacitor, particularly for surface mount applications. SMT ceramic capacitors greater than 47 μ F are less commonly available.

11. FINE TUNING RG, RL, AND CL

The R_{g} , R_{L} , and C_{L} component values can be fine-tuned experimentally. Start with component values from Table 2, and operate the temperature controller system to determine if the load temperature settling time is satisfactory. If it is not, then follow these steps to fine-tune the component values.

- 1. Short C_1 to remove the integrator term.
- 2. Increase the proportional gain k_p by increasing R_L until the temperature begins to oscillate; this is the Critical Gain value of the system. Measure the period of the oscillations in seconds.
- 3. Decrease R_{L} by half.
- Use Equation 5 to calculate R_G and C_L so that the value of t_C is slightly greater than the oscillation period measured above.

12. INCREASING OUTPUT CURRENT DRIVE

The WHY5640 is specifically designed to operate in a master/slave output current boosting configuration. Two or more WHY5640 controllers can be coupled to boost the output current.

Figure 15 shows how to connect two WHY5640 controllers together to increase the output current drive to 4.4 Amps.

Pin 4 (BUFA) and Pin 14 (BUFB) provide buffered outputs of Pin 3 (LIMA) and Pin 2 (LIMB), respectively. The slave controller is controlled by the master controller by connecting Pin 4 (BUFA) of the master unit to Pin 3 (LIMA) of the slave unit. Similarly, Pin 14 (BUFB) of the master unit then connects to Pin 2 (LIMB) of the slave unit. Each successive slave unit uses its buffered out-puts, Pins 4 and 14, to drive the next slave units output drive section via its Pins 3 and 2. The master controller sets the current limits for all successive slave controllers connected to the master controller, requiring only one set of heat and cool limit resistors.

Use Table 3 to determine the limit setting resistors, $\rm R_A$ and $\rm R_B$, based on the number of WHY5640 controllers paralleled together.

Table 3

Current Limit Set Resistor vs Maximum Output Current vs Number of Paralleled WHY5640 Controllers.

Maximum Output Current (Amps)

1 WHY5640 Controller	2 WHY5640 Controllers	3 WHY5640 Controllers	4 WHY5640 Controllers	5 WHY5640 Controllers	Limit Set Resistor (kΩ)
0	0	0	0	0	1.60
0.1	0.2	0.3	0.4	0.5	1.69
0.2	0.4	0.6	0.8	1	1.78
0.3	0.6	0.9	1.2	1.5	1.87
0.4	0.8	1.2	1.6	2	1.97
0.5	1	1.5	2	2.5	2.08
0.6	1.2	1.8	2.4	3	2.19
0.7	1.4	2.1	2.8	3.5	2.31
0.8	1.6	2.4	3.2	4	2.44
0.9	1.8	2.7	3.6	4.5	2.58
1	2	3	4	5	2.72
1.1	2.2	3.3	4.4	5.5	2.88
1.2	2.4	3.6	4.8	6	3.05
1.3	2.6	3.9	5.2	6.5	3.23
1.4	2.8	4.2	5.6	7	3.43
1.5	3	4.5	6	7.5	3.65
1.6	3.2	4.8	6.4	8	3.88
1.7	3.4	5.1	6.8	8.5	4.13
1.8	3.6	5.4	7.2	9	4.42
1.9	3.8	5.7	7.6	9.5	4.72
2	4	6	8	10	5.07
2.1	4.2	6.3	8.4	10.5	5.45
2.2	4.4	6.6	8.8	11	5.88
2.3	4.6	6.9	9.2	11.5	6.36



Figure 15





13. HELPFUL HINTS

Selecting a Temperature Sensor

Select a temperature sensor that is responsive around the desired operating temperature. The temperature sensor should produce a large sensor output for small changes in temperature. Sensor selection should maximize the voltage change per °C for best stability.

Table 4 compares temperature sensors versus their ability to maintain stable load temperatures with the WHY5640.

Mounting the Temperature Sensor

The temperature sensor should be in good thermal contact with the device being temperature controlled. This requires that the temperature sensor be mounted using thermal epoxy or some form of mechanical mounting and thermal grease.

Avoid placing the temperature sensor physically far from the thermoelectric. This is typically the cause for long thermal lag and creates a sluggish thermal response that produces considerable temperature overshoot.

Mounting the Thermoelectric

The thermoelectric should be in good thermal contact with its heatsink and load. Contact your thermoelectric manufacturer for their recommended mounting methods.

Table 4

Temperature Sensor Comparison of voltage change per degree C.

SENSOR Thermistor		RTD	AD590	LM335
RATING	Best	Poor	Good	Good

Heatsink Notes

If your device stabilizes at temperature but then drifts away from the setpoint temperature towards ambient, you are experiencing a condition known as thermal runaway. This is caused by insufficient heat removal from the thermoelectric's hot plate and is most commonly caused by an undersized thermoelectric heatsink.

Ambient temperature disturbances can pass through the heatsink and thermoelectric and affect the device temperature stability. Choosing a heatsink with a larger mass will improve temperature stability.



CERTIFICATION AND WARRANTY CERTIFICATION:

Wavelength Electronics, Inc. (Wavelength) certifies that this product met it's published specifications at the time of shipment. Wavelength further certifies that its calibration measurements are traceable to the United States National Institute of Standards and Technology, to the extent allowed by that organization's calibration facilities, and to the calibration facilities of other International Standards Organization members.

WARRANTY:

This Wavelength product is warranted against defects in materials and workmanship for a period of 90 days from date of shipment. During the warranty period, Wavelength will, at its option, either repair or replace products which prove to be defective.

WARRANTY SERVICE:

For warranty service or repair, this product must be returned to the factory. An RMA is required for products returned to Wavelength for warranty service. The Buyer shall prepay shipping charges to Wavelength and Wavelength shall pay shipping charges to return the product to the Buyer upon determination of defective materials or workmanship. However, the Buyer shall pay all shipping charges, duties, and taxes for products returned to Wavelength from another country.

LIMITATIONS OF WARRANTY:

The warranty shall not apply to defects resulting from improper use or misuse of the product or operation outside published specifications.

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EXCLUSIVE REMEDIES:

The remedies provided herein are the Buyer's sole and exclusive remedies. Wavelength shall not be liable for any direct, indirect, special, incidental, or consequential damages, whether based on contract, tort, or any other legal theory.

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NOTICE:

of Wavelength.

tures are maintained.

life support device.

REVISION DATE

Feb-08

31-Aug-09

3-Jun-11

16-Dec-11

2-Apr-12

REV. H

REV. I

REV. J

REV. K

REV. L

LIFE SUPPORT POLICY:

SAFETY:

The information contained in this document is

subject to change without notice. Wavelength

will not be liable for errors contained herein

or for incidental or consequential damages in

connection with the furnishing, performance, or

use of this material. No part of this document

may be photocopied, reproduced, or translated to

another language without the prior written consent

There are no user serviceable parts inside

this product. Return the product to Wavelength

for service and repair to ensure that safety fea-

As a general policy, Wavelength Electronics, Inc.

does not recommend the use of any of its products

in life support applications where the failure or

malfunction of the Wavelength product can be

reasonably expected to cause failure of the life

support device or to significantly affect its safety

or effectiveness. Wavelength will not knowingly

sell its products for use in such applications

unless it receives written assurances satisfactory

to Wavelength that the risks of injury or damage

have been minimized, the customer assumes all such risks, and there is no product liability for

Wavelength. Examples of devices considered to be

life support devices are neonatal oxygen analyzers,

nerve stimulators (for any use), auto transfusion

devices, blood pumps, defibrillators, arrhythmia detectors and alarms, pacemakers, hemodialysis

systems, peritoneal dialysis systems, ventilators of

all types, and infusion pumps as well as other

devices designated as "critical" by the FDA. The above are representative examples only and are not

intended to be conclusive or exclusive of any other

REVISION HISTORY

NOTES

diagram

Updated formatting

Updated mechanical dimensions and links to

support new website

Updated mechanical specifications

Updated Proportional

Constant calculations

Gain and Integrator Time

Added Quick Connect

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